Seismic Design of Bridges for Continued Functionality Using Seismic Isolation

Western Bridge Engineers' Seminar September 25-28, 2011 by Roy A. Imbsen, D.Engr., P.E .

AASHTO Adopted 2009 Guide **Specifications**

Proposed

AASHTO Guide Specifications for LRFD Seismic **Bridge Design**

Subcommittee for Seismic Effects on Bridges $T-3$

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Guidelines(7.1)-General Seismic Load Path and Affected Components

Guidelines(7.2) Performance Criteria

- ♦ Type 1 Design a ductile substructure with an essentially elastic superstructure (i.e., yielding columns)
	- 1 concrete substructure
	- 1* steel substructure
	- 1** concrete filled steel pipe substructure
- ♦ Type 2 Design an essentially elastic substructure with a ductile superstructure (i.e., steel girder bridge with buckling diagonal members in the end diaphragms.
- ♦ Type 3 Design an elastic superstructure and substructure with a fusing (e.g., isolation) mechanism at the interface.

Type 1 - Design a ductile substructure with an essentially elastic superstructure (i.e., yielding columns)

- 1 concrete substructure
- 1* steel substructure
- -1** concrete filled steel pipe substructure

New Zealand Small Column Test

Plastic Hinging of Column An Affordable Approach

Calibration Objectives

Global Design Strategies Type 2 Design

Type 2 - Design an essentially elastic substructure with a ductile superstructure (i.e., steel girder bridge with buckling diagonal members in the end diaphragms.

Global Design Strategies Type 3 Design

Type 3 - Design an elastic superstructure and substructure with a fusing (e.g., isolation) mechanism at the interface.

Current State of Practice for Seismic Design of Bridges

- Ductile based design
- ♦Life Safety (i.e. Collapse Prevention) using ductile design with damage allowed. Continued Functionality is not achieved.
- ♦Non-functional bridges following a major earthquake

Structure Damage Occurs Because

- ♦Seismic codes allow damage for strong earthquakes.
- ♦Severe earthquakes can cause force and displacement demands several times greater than that required by the design criteria.
- When demands exceed the structural design strength, linear elastic dynamic analyses are at best only approximations.
- ♦Large deformations concentrate in the weakest structure members, causing damage, and sometimes collapse.

The Cost To Rebuild After Major Earthquakes is Many Times Greater Than The Costs To Build Before The Earthquake.

Calibration Objectives

How can we have higher Reliability for a Bridge to be Functional for a design life of 75 or 100 Years?

- ♦Responding structure to remain fully elastic (i.e., Reliably Elastic)
- ♦Functional seismic connections and joints

♦We now have the technology to design and build a functional bridge at a lower construction cost than designing and building to minimum code requirements

Objectives for Continued **Functionality**

- ♦Satisfy Service Load Requirements
- Isolate the Substructure from the Superstructure
- ♦Keep the Substructure Columns Reliably Elastic During an MCE (e.g.1000 year event)
- ♦Precludes the Formation of a Plastic Hinge (i.e. no damage)
- ♦Eliminates the Capacity Protection Required for the Foundation

AASHTO Specifications 2009 and Guide Specifications 2009

2009 Interim Revisions

AASHTO LRFD Bridge Design Specifications

> **Customary U.S. Units 4th Edition** 2007

American Association of State Highway and Transportation Officials

AASHTO LRFD Bridge Design

1.3.3 Ductility

The structural system of a bridge shall be proportioned and detailed to ensure the development of significant and visible inelastic deformations at the strength and extreme event limit states before failure *i.e.*, Damage

Energy-dissipating devices may be substituted for conventional ductile earthquake resisting systems and the associated methodology addressed in these Specifications or in the AASHTO Guide Specifications for Seismic Design of Bridges. i.e., No Damage

2009 Interim Revisions

AASHTO LRFD Bridge Design Specifications

Customary U.S. Units 4th Edition 2007

American Association of State Highway and Transportation Officials

AASHTO **Specifications** 2009 & 2010

Guide Specifications for Seismic Isolation Design Third Edition July 2010

Types of Seismic Isolation Systems Used In USA

- ♦Lead Core Rubber
	- –*Dynamic Isolation Systems, Inc.*
	- –*Seismic Energy Products, L.P.*
- ♦EradiQuake
	- –*R.J. Watson, Inc.*
- ♦Friction Pendulum
	- –*Earthquake Protection Systems, Inc.*

Note: High-Damping Rubber is not used

Lead Rubber Bearing

Energy Dissipation Core

Friction Pendulum Bearings

Triple Pendulum Bearing

Friction Pendulum Bearing

13. Required Tests for Isolation

"All isolation systems shall have there seismic performance verified by Testing"

• System Characterization ◆ Prototype ♦Quality Control

Selection Of An Isolation System

- ♦Service loads and movements
- ♦Axial load, sliding systems have more capacity
- ♦Available height and/or space
- ♦Displacement demands
- ♦Temperatures

California 's High Speed –Rail System

California High-Speed Train Project

TECHNICAL MEMORANDUM

Structure Design Loads TM 2.3.2

TECHNICAL MEMORANDUM

Interim Seismic Design Criteria Bridges and Aerial Structures, Tunnels and Underground Structures, Passenger Stations and Building Structures TM 2.10.4

TECHNICAL MEMORANDUM

Track-Structure InteractionTM 2.10.10

1.2 STATEMENT OF TECHNICAL ISSUE

♦The provisions of this Technical Memorandum were developed using a ductility design concept with a plastic hinge forming at the fixed-end support of a column. The performance achieved using this concept is "Life Safety" (i.e. no collapse). Severe damage is permitted to occur in the plastic hinge region as long as structure collapse is prevented.

Seismic Isolation Design Study

Load Case Combinations

- DL: Dead load of structural components and permanent attachments
- LF: Traction or braking force
- I: Vertical impact effect
- MCE: Maximum Considered Earthquake
- LDBE: Lower-Level Design Basis Earthquake
- (LLRM + I) multiple tracks of (LLRM + I)

Test-Design Parameters (100 ft. span)

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1.2 STATEMENT OF TECHNICAL ISSUE

♦For elevated structures supporting nonredundant high-speed rail systems higher performance levels having minimum or no damage with Continued Functionality is expected and can be achieved. This is particularly important requirement for the CHSRS to satisfy the expectations of the user community and to satisfy revenue generation commitments.

TECHNICAL MEMORANDUM

Seismic Design Criteria with Recommended Revisions for **Continued Functionality**

Structures Supporting High-Speed Trains TM 2.10.4

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California High-Speed Rail Program Management

Figure 1: 38' Column Height SAP Model

Objectives

- ♦Satisfy Service Load Requirements
- Isolate the Substructure from the Superstructure
- Keep the Substructure Columns Elastic During an MCE (1000 year event)
- ♦Precludes the Formation of a Plastic Hinge (i.e. no damage)
- ♦Eliminates the Capacity Protection Required for the Foundation

Lets' Take the Next Step Raise the Bar for Seismic Protection

- ♦Continued Functionality
- ♦Increased Reliability at Lower Construction Costs \$\$\$\$
- ♦Increased Performance No Damage
- ♦Implement Current Technology using Isolation

Thank You

Earthquake Protection Systems

